

Heat Move using Light Weight Total in Concrete

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ABSTARCT

LWC and LWA are different from one another in terms of mechanical, durability, as well as thermal performance (NWC). LWC's heat capacity and thermal conductivity are challenging to measure since the components, combination proportions, and moisture states of the material have not been well researched. A variety of SLWC, ALWC, and NWC combinations as well as a variety of lightweight and normal-weight grout formulations were evaluated in this study. Studying concrete and grout combinations with this LWA was done and compared to past findings. The statistical models used have an effect on the enlarged slate LWA's thermal conductivity and heat capacity.

Keywords: Thermal conductivity, heat capacity, lightweight aggregate, and other terms used to describe the characteristics of heat

1. INTRODUCTION

Construction, design, and construction of both buildings and vehicles are affected by concrete's thermal performance. For accurate temperature profiles and heat flow measurements, it is necessary to understand the thermal properties of concrete. There are several other important criteria to consider when looking at the thermal performance of concrete buildings, in addition to CTE (such as dimensional stability, cracking resistance and insulation). 1 Structural and pavement engineers utilize thermal parameters like thermal conductivity and heat capacity to quantify heat flow and storage. Material thermal conductivity is a measure of its capacity to retain heat and reduce temperature fluctuations. Having a lower heat conductivity is linked to better insulate. 2 Building energy consumption can't be analyzed without taking into account these two factors.

1.1 Background

Both the individual components' individual thermal characteristics as well as any free space in the concrete mix affect its overall thermal properties. There are several variables that impact the thermal conductivity of concrete, including its age, volume fraction of aggregate, cement concentrations, admixtures, fine aggregate content, temperature and moisture content. 8 Many variables influence concrete's thermal conductivity, including the temperature, moisture content, density, and volume percent of aggregate. 8 Concrete's thermal characteristics are greatly affected by the aggregate, which normally makes about 60 to 70 percent of the volume of concrete. a total of one, nine According to Lane, the thermal performance of LWC when LWAs are added into concrete mixes is influenced when synthetic aggregates like LWAs have different thermal characteristics than natural aggregates like rocks and minerals (NWC). Because of its internal curing properties, 10 LWAs are becoming increasingly popular for use in construction and bridge building projects. The porosity of expanded LWAs can vary greatly depending on the raw material, the type of thermal treatment used to induce expansion, and how it is cooled, crushed, or graded throughout manufacture. Because "air voids and moisture content disguise the effects aggregate type," the thermal performance of LWC is directly linked to LWA porosity. 4

2. Modeling thermal properties and performance

All structural analysis models, whether they are used in building energy simulation models or pavement design tools, must accurately characterize the material's thermal characteristics. Due to concrete's thermal performance being affected by porosity, early forecasts used unit weight. Valore established a simple exponential model for the correlation between density and thermal conductivity. For the prediction of concrete's thermal conductivity, Campbell-Allen and Thorne¹⁵ employed a two-phase theoretical model that included both mortar and aggregate. Bhattacharjee and Krishna-moorthy⁹ have proposed an idealized system of "enclosing and enclosed pores" for porous materials' thermal conductivity, although Harmath⁹ refers to analogous two- and multi-phase models. The accuracy of other researchers' neural network models for estimating concrete's thermal conductivity has been demonstrated using real data values.

Concrete's thermal conductivity and heat capacity have been empirically examined in a number of publications using typical, standard-weight concrete or mortar particles (NWA's). Mortar and concrete's thermal conductivity is connected to the kind and moisture state of the particles used in construction, according to new research. These include specimen ages, water-cement ratios, admixtures, coarse and fine aggregate quantities [CFA], ambient temperatures and humidity levels, among others were examined in a study⁸ by Kim et al.⁷

2.1 Published thermal properties

ACI 122R-14 provides a range of values for the thermal conductivity and heat capacity of concrete that may be used for engineering purposes. Temperature data for popular construction and insulation materials is provided by ASHRAE in their Handbook of Heating, Refrigeration and Air-Conditioning Engineers (ASHRAE). The density of concrete is used to get suggested

values for concrete's thermal characteristics. When referring to Valore, these values may be found in Table 1. Table 1 shows that the suggested values of heat conductivity for concrete of various densities have a large amount of overlap. The value of a property is greatly influenced by its density. An experienced designer would have difficulty selecting the ideal mix of local components and projected proportions from Table 1. During testing, the moisture content of the concrete and the type of aggregates used were not recorded in this report.

When it comes to the properties of wet concrete, ASTM STP 169D, Significance Of Tests And Properties Of Concrete And Concreting Materials, the difference is just 0.62 W/(h·ft·°F). There was a tiny difference between these values and ASTM STP 169D specimen preparation, specimen preparation, and moisture conditions in the 1960s when these values were established; these values give no more information on the specimens used in ASTM STP 169D (particularly for higher-strength mixtures). Like ASTM STP 169D, this standard does not offer heat capacity data in terms of unit weight or moisture content. The thermal conductivity of concrete ranges from 0.70 to 0.70 Btu/(h·ft·°F) in a study by Lee et al.¹⁷. If the global default is set to 1.73 W/m·K, the temperature conductivity of regular pavement concrete can be used between 1.0 and 2.60 W/m·K.

Table1—Concrete's typical thermal characteristics (from ASHRAE24)

Material	Density, kg/m ³ (lb/ft ³)	Thermodynamics, W/(m·K) (Btu/(h·ft·°F))	Heat capacity (weight basis), J/(kg·K) (Btu/(lb·°F))
Normal weight concrete (sand and gravel or stone aggregates)	2400 (150)	1.4 to 2.9 (0.83 to 1.67)	Not provided
	2240 (140)	1.3 to 2.6 (0.75 to 1.50)	800 to 1000 (0.19 to 0.24)
	2080 (130)	1.0 to 1.9 (0.58 to 1.08)	Not provided
Concrete made with light-weight aggregate (pumice and scoria; expanded slag, clay, slate, pumice, and scoria)	1920 (120)	0.9 to 1.3 (0.53 to 0.76)	840 (0.20)
	1600 (100)	0.68 to 0.89 (0.39 to 0.52)	Not provided
	1280 (80)	0.48 to 0.59 (0.28 to 0.34)	
	960 (60)	0.30 to 0.36 (0.17 to 0.21)	
	640 (40)	0.18 (0.11)	

1.25 Btu/(h·ft·°F) at a power density of 2.16 W/(m·K) 6 An acceptable range for thermal conductivity of ordinary concrete in M-EPDG is 840 to 1680 J/(kg·K) (0.20 to 0.40 Btu/(lb·°F) for the default value of 1170 J/(kg·K). 6

3. RESEARCH OBJECTIVES

Rather of using NWA, expandable slate should be used to better understand thermal conductivity and thermal capacity (non-expanded slate). Data from LWC thermal modeling may be utilized to improve the model. There were a range of amounts used in the experiment of cement, cementitious materials, sand and aggregates, as they were all consistent with the components (Cement, cementitious materials, and fine aggregate, for instance). Moisture content was minimized utilizing normal specimen conditioning for thermal testing on bulk specimens. Void content had an immediate impact on thermal conductivity and heating capacity when compared to unit weight, according to the results of this study LWA volume and total void content have been demonstrated to be linked with total void content (aggregate pores plus the air content detected) (aggregate pores). These researchers looked at a wide range of thermal properties in a number of real-world situations. For example, the way they conduct heat would be drastically changed.

3.1 Test results for concrete mixes and their early ages

Structural, roadway, and masonry applications all benefit from the widespread usage of common concrete and grout combinations. Compressive strengths of various groups were affected by changes in cement volume and water cementitious materials ratios (w/cm). A higher compressive strength than the minimum values listed here is expected. There was no bad aggregate in the grout at all. For the purposes of this study, the most common structural concrete mixtures used were included in Table 3, together with their mix designations and proportions, as well as the results of tests on both fresh and hardened concrete quality (a). Concrete mixes, both fresh and hardened, are mentioned frequently. Table 2 shows that aggregates are a prevalent component of study mixes, as shown.

Characteristic	Coarse aggregates		Fine aggregates	
	Normal weight	Lightweight	Normal weight	Lightweight
Type	Granitic gneiss	Expanded slate	Natural silica sand	Expanded slate
Gradation	ASTM C33 or AASHTON M 67	ASTM C330 or AASHTOM 195*	ASTM C33	NCDOT 2MS
Specific gravity	2.75	(6 mm) in diameter is the maximum No more than half an inch in diameter can be used	2.63	1.85
Absorption, %	0.50	at a maximum of 6.0 at the end of 24 hours reaching a maximum of 7.0 throughout the course of 24 hours	0.50	10.0 (at 24 hours)
Bulk loose unit weight, kg/m ³ (lb/ft ³)	1506 (94)	801 (50)	1474 (92)	881 (55)

Both structural and DOT mixtures are permitted to have nominal maximum diameters of 19.05 mm (3/4 in.) and 12.7–mm (1/2 in.). Consider that one inch equals 25.4 mm, so keep that in mind. Table 3 lists the parameters of roadway (DOT) and grout mixtures (b).

Fresh and hardened concrete testing

Measurements of slump, air content, and unit weight of fresh-mixed concrete were made using volumetric ASTM C143 and ASTM C173 methods, respectively (ASTM C138). Results of these tests are shown in Table 3. For the most part, the higher-strength mixes included water-reducing admixtures, resulting in larger slumps of 102–254 mm (4–10 in.). Scales calibrated to measure fresh unit weights were utilized. ASTM C127 methods were used to measure the oven-dry densities of hardened concrete in the form of 4-inch diameter x 8-inch length cylindrical specimens. A density of 50 kg/m³ (3 lb/ft³) was used to compute the equilibrium density. Using a unit-weight bucket to test concrete density results in a slightly different density than using a unit-weight cylinder. The average percentage of air in the room was 5.5% to 1%. Additionally, the results of tests on compressive strength performed after seven and 28 days are shown in Table 3. (ASTM C39). It was necessary to cast and cure cylindrical specimens with a diameter of 4 inch and an overall length of 8 inch for each mixture before they could be demolded. Specimens were cured in lime-water curing baths in accordance with ASTM C192 prior to testing, if required. After 28 days of testing, only two of the tested combinations failed to reach the necessary minimum concrete compressive strength, as indicated in Table 3. ALWC 4000 and ALWC 5000, despite their lower-than-anticipated compressive strengths, were able to withstand a steady increase in compressive strength due to the mixture proportions utilized. Because of the new curing method in ASTM C330, it's possible that compressive strengths have increased.

Computed void content of concrete

Concrete, for example, has a significant effect on how a building's temperature responds when it is utilized. To better understand and maybe predict the thermal performance of concrete, a reasonable estimate of the total void content must be established. As a result of the aggregate's lack of porousness, typical concrete's holes are filled with air. In order to determine the amount of trapped and entrained air in the paste, normal air content test methodologies must be used, which do not reveal the aggregate void count. This necessitates the employment of a different method to calculate the LWC's total volume of voids.

Thermal test methods

Samples were cut from standard cylinder specimens to measure thermal conductivity and heat capacity. Figure 1a shows the dimensions of the prisms, which were 1.5 inches thick, 38.1 inches wide, and 1.5 inches tall. Each mixture was tested with nine specimens in total, three specimens from each of the three distinct containers. The samples were stored in an environmental room at 22.2°C (72°F) and 50% relative humidity for seven days prior to testing. Following their removal from the environmental room, specimens were wrapped in plastic and maintained there until they were ready to be analyzed in the laboratory once again. Heat flow meters were utilized to measure the material's steady-state thermal transmission properties, such as conductivity and heat capacity, as seen in Fig. 1(b). A software program oversees the device's calibration and testing. To ensure accurate results, the calibration method was performed both before and after testing, using a reference sample.

provided by the manufacturer. Results included a device-calculated correction for specimen thickness throughout each run. Pads were used to protect the specimens while providing excellent contact with heating elements and sensors while employing a test chamber, as seen in this figure. At 25°C (77°F), the thermal conductivity result was obtained using two temperature settings: one set at 20°C (68°F) and the other set to 30 °C (86 °F). To produce heat in a specific area and software.

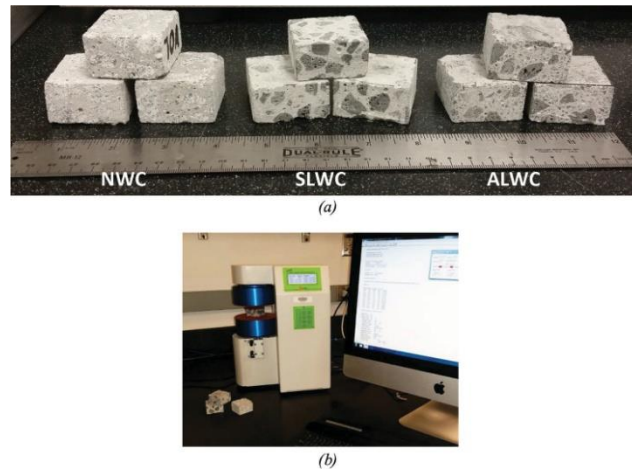


Figure:1—(a)sample often used in the measurement of heat capacity and thermal conductivity; and a device for measuring heat flow

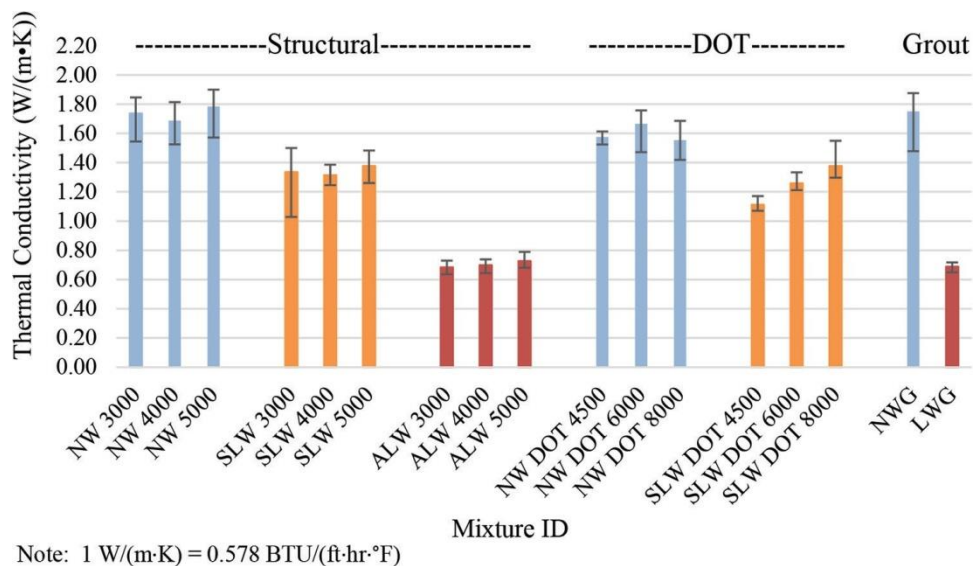


Figure 2 displays information on thermal conductivity.

At 20 degrees Celsius and 30 degrees Celsius, we achieved the expected outcomes. " Pads and parchment paper used to protect sensor coatings had their thermal characteristics considered while determining test results

4.RESULTS

4.1 Thermalconductivity

A decrease in conductivity with increasing LWA concentration and an increase in conductivity with increasing strength were predicted based on the literature study. Each of the nine specimens evaluated for each mixture is represented by a range bar in Fig. 2, which shows the average of the test findings for each mixture. Thermal conductivity of all combinations was shown to be significantly affected by the replacement of expanded LWA for NWA in the concrete mixtures studied. Thermal conductivity of concrete mixes with LWA is significantly reduced, indicating the possibility for improved insulation performance, as predicted. Figure 2 demonstrates that the thermal conductivity values were significantly influenced by the substitution of LWA for NWA rather than the higher cement content or other considerations.

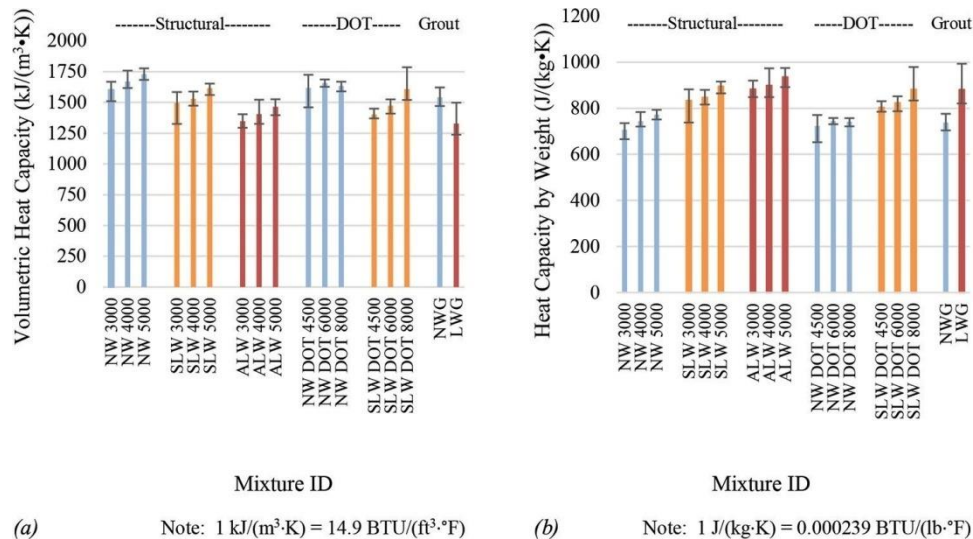


Figure 3—(a) As a result of volumetric heat capacity,;and(b)heatcapacity(byweight)results.

alterations in the composition of the mixture are necessary to enhance the compressive strength. A correlation between increased heat conductivity and increased cement content appears to exist only for the SLW DOT blends studied. There was a 77 percent efficiency gap between NWC mixes and SLWC combinations in terms of thermal conductivity ($1.736 \text{ W}/(\text{m}\cdot\text{K})$ ($1.003 \text{ Btu}/(\text{h}\cdot\text{F})$), yet the thermal conductivity of NWC mixtures was still 77 percent higher than that of SLWC combinations. ALWC and NHWC concrete results in a 60% reduction in heat conductivity compared to the usual NWC concrete mixture, roughly 40% lower. M-default EPDG's range of $2.16 \text{ W}/(\text{m}\cdot\text{K})$ equals $1.25 \text{ W}/(\text{h}\cdot\text{ft}^2\cdot\text{F})$. But the M-default EPDG's range of $2.16 \text{ W}/(\text{m}\cdot\text{K})$ is far lower than these values. On the upper end of their range, these SLWC structural and roadway combinations were estimated to weigh around $1762 \text{ kg}/\text{m}^3$ ($110 \text{ lb}/\text{ft}^3$) For $1538 \text{ kg}/\text{m}^3$ ($96 \text{ lb}/\text{ft}^3$), Table 1 shows that the thermal conductivity values for the ALWC combinations were closer to the middle of the expected range. With an average thermal conductivity of $0.41 \text{ Btu}/(\text{h}\cdot\text{ft}\cdot\text{°F})$ for ALWC mixtures as a reference, the provided statistics may not accurately reflect combinations made with local materials.

Heatcapacity

Two operational definitions are used to determine a device's heat capacity. Building energy analysis uses mass concrete's heat capacity as a weighted average of the volumetric capacity. In this inquiry, volumetric heat capacity test data is reported for the equipment used. As can be seen in Fig. 3(a), Results from the heat capacity tests show the maximum and minimum values for each specimen tested for each of the nine mixes. Thermal conductivity was more affected than heat capacity when LWA was substituted for NWA. This material's heat storage properties, as well as its void content, are discussed in further detail in other resources recommended to the reader. These resources include: conduction, convection, and radiation. 28 To illustrate, Table 1 shows the average volumetric heat capacity for each series of combinations as compressive strength (and cement concentration) increases. As can be seen from the measured value ranges, there is a great deal of overlap among the mixes within each sequence. The volumetric heat capacity impact of LWA should be shown by comparing NWC and SLWC mixtures.

NWC mixes have a volumetric heat capacity of $1670 \text{ kJ}/(\text{m}^3\cdot\text{K})$, which is 7.2 percent and 15.7 percent lower than the average volumetric heat capacity of SLWC and ALWC mixtures, which are both $1550 \text{ kJ}/(\text{m}^3\cdot\text{K})$ and $1400 \text{ kJ}/(\text{m}^3\cdot\text{K})$ respectively. NWC and SLWC combinations have lower average volumetric heat capacities than their individual constituents, at $1640 \text{ kJ}/(\text{m}^3\cdot\text{K})$ ($24,500 \text{ Btu}/(\text{ft}^3\cdot\text{°F})$), which is an important point to keep in mind. The regular weight grout's average volumetric heat capacity (which is $1540 \text{ kJ}/(\text{m}^3\cdot\text{K})$; $23,000 \text{ Btu}/(\text{ft}^3\cdot\text{°F})$) drops by 13.9 percent when compared to the lightweight grout's $19800 \text{ Btu}/(\text{ft}^3\cdot\text{°F})$ average heat capacity. ANALYSIS

When using regression analysis to uncover patterns in the data, we looked at thermal conductivity (as well as volumetric heat capacity) and heat capacity per weight (as well as unit weight) (dependent variables). We can see clusters of points corresponding to the three types of mix- tures in the figures that exhibit these results, illustrating the importance of void content in terms of these thermal characteristics. The built-in regression tools in Excel are used to draw trendlines, which show the statistical correlations between the independent and dependent variables. R2 values can be marginally improved using higher-level quadratic models, however there is no physical rationale for this model. The influence of LWA on these attributes can be better understood with the use of trendlines.

5.CONCLUSIONS

Changes to concrete's thermal conductivity result in a significant reduction in its thermal conductivity. There are considerable discrepancies between M-EPDG pavement design requirements and suggested design values and aggregate quantities in concrete mixes using LWA expanded slate, coarse granitic limestone, and natural silica. Our findings show that thermal characteristics have more of an impact on the overall void content of the mixture (such as cement content) than other mixture components (such as w/cm) or proportioning parameters (such as LWA). All of the steps were simple and straightforward.

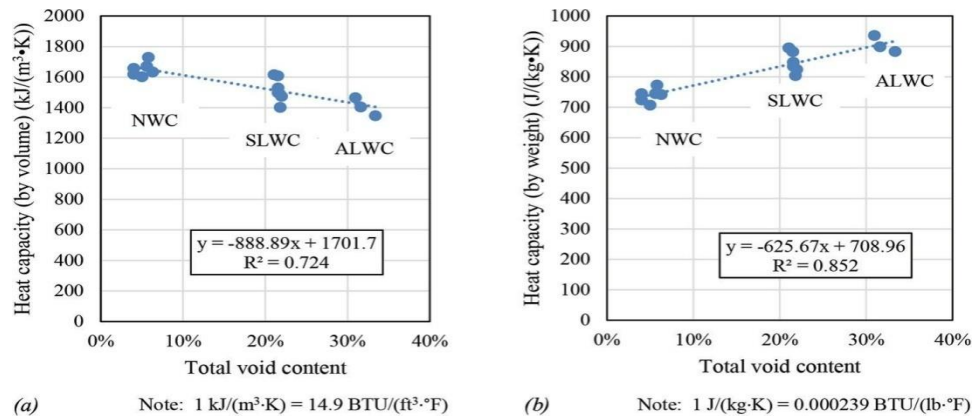


Figure:6—(a)Volumetric heat capacity and void content have a relationship.and(b)connection between weight and heat capacity by volume void content

For highway NWC combinations, ASHRAE's suggested range of values did not apply. SLWC and ALWC blends also did not fall inside this range. The heat capacity test findings (M-EPDG) for DOT combinations are below the acceptable range, whereas those for SLW DOT mixtures are within the recommended range. For more accurate results, measurements should be utilized instead of those found in published literature. Calculating a material's heat capacity and thermal conductivity may be done using the total void content and weight per unit area (W/kg). LWA Designers may be interested in the correlations between the thermal characteristics of concrete mixtures with comparable constituents (expanded slate LWAs).

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